

## CHAPTER VI

### BUILDING HEAT GAIN AND HEAT LOSS SIMULATIONS

In this chapter building heat gain and heat loss through walls, roof and windows were simulated using a computer model and the hourly weather data set which was prepared through Chapter V. Then, the output data were analyzed to identify the optimum building shapes for 16 different building orientations in Oklahoma City area.

#### 6.1 Description of the Computer Model

A computer model for calculating building heat gain and heat loss was developed by applying the ASHRAE methods discussed in Chapter IV. This model was written in Microsoft QuickBASIC language for IBM-PC and its compatible machines.

For the calculation of building heat gain and heat loss, the following assumptions were made.

- 1) The building was assumed to be a box-shaped one-room enclosure.
- 2) The various external walls, roof and windows were treated as separate heat flow paths.

3) The conduction heat transfer through building components was assumed to be one-dimensional.

4) The heat transfer coefficients for the inside and outside surfaces of the building were considered constant.

5) All building materials were assumed to be homogeneous, having constant thermal and physical properties.

6) The temperature distribution inside the building were considered uniform.

7) The indoor design temperatures were set to 75 °F in cooling season and 70 °F in other season.

The main procedure of calculating heat gain and heat loss through building envelope includes:

- 1) input of building dimensions, materials and glass properties,
- 2) input of hourly weather data,
- 2) calculating hourly wall-solar azimuth angles and solar incident angles on walls,
- 3) calculating hourly total solar radiation on each building surface,
- 4) calculating hourly sol-air temperatures on roof and walls,
- 5) calculating transmission coefficient of each window using the hourly solar incident angle on the window,
- 6) calculating heat gain or heat loss through windows,
- 7) calculating conductive heat gain or heat loss through roof and walls,
- 8) and output of heat gain or loss amounts.

The procedures for calculating actual heating or cooling load and internal heat gain were not included because of the following reasons.

1) The use of this computer model was to produce the data for the comparison of the heat flow amount which would be different among the buildings having different length-to-width ratios and orientations. The comparison of heat flow amount through building envelope, as Olgyay did, might be enough to identify an optimum building shape for a given orientation of that building.

2) The buildings were assumed to have same use, number of occupants and amount of internal heat sources. So, the internal heat gain were assumed to be identical in the buildings.

Table 6.1 shows the input data for the heat gain and heat loss simulations. Among the data, those thermal transfer function coefficients of different materials for roofs and walls were taken from ASHRAE Handbook of Fundamentals 1977, and recorded on disk files. So, the values can be read by the program according to the ASHRAE roof and wall numbers specified in the input procedure. A box-shaped building having floor area of 1000 ft<sup>2</sup> and wall height of 10 ft was assumed. Then, total 41 different building shapes were pre-defined in terms of the building width-to-length ratios from 5:1 to 1:5.

Table 6.2 shows the actual building widths and lengths which constitute floor area of 1000 ft<sup>2</sup>. In this study, in lieu of the conventional terms for walls, such as south, north, east and west walls, the terms of front, back, left and right walls were used because of the changing orientations of the main window wall which was called



## 6.2 Simulation Procedure

From the input data, building heat gain and heat loss in Oklahoma City area were determined through a series of computer simulations.

For the computer simulations, sixteen IBM-AT compatible machines<sup>1</sup> were employed at a time. One of the 16 different orientations was given to each machine and 8760 hours' heat gain and loss were simulated.

First of all, hourly total solar radiation intensity on each building surface was calculated from the hourly solar radiation values on a horizontal surfaces which were recorded in the weather data set. Tables 6.3.1 through 6.3.4 show the hourly solar radiation intensities on a unit surface area (BTU/h/ft<sup>2</sup>) of the roof and walls of 16 different orientations on March 21, June 21, September 21 and December 21, respectively. And figures 6.1.1 through 6.4 show the plots of these values. As shown in the figures, the hourly solar radiation intensities on the walls vary in connection with the sun positions, cloud cover ratios and wall orientations.

The hourly heat gain and loss (BTU/h) values were calculated by summing those through the roof, walls and windows. Then, the hourly values were accumulated separately in gain and loss to get daily sums of heat gain and heat loss (BTU/24hrs). Again, the daily sum values were added up to get monthly sums of heat gain and heat loss (BTU/month). Finally averages of daily heat gain and heat loss (BTU/day) were calculated

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<sup>1</sup> These machines were equipped with 10 MHz INTEL 80286 processors and 80287 numeric Co-processors. About 6 hour running time was needed to complete a 8760 hours' heat gain and heat loss simulation on one machine.

by dividing the monthly sum by the total number of days in each month.

Table 6.3.1 March 21. Hourly solar radiation on unit surface area [BTU/h/ft<sup>2</sup>]

| TM | CC | N  | NNE | NE | ENE | E  | ESE | SE | SSE | S  | SSW | SW | WSW | W  | WNW | NW | NNW | RF  |
|----|----|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|-----|
| 7  | 9  | 16 | 16  | 32 | 46  | 55 | 59  | 55 | 46  | 33 | 16  | 16 | 16  | 16 | 16  | 16 | 16  | 29  |
| 8  | 9  | 32 | 32  | 41 | 54  | 64 | 69  | 68 | 62  | 51 | 38  | 32 | 32  | 32 | 32  | 32 | 32  | 62  |
| 9  | 10 | 37 | 37  | 37 | 37  | 37 | 37  | 37 | 37  | 37 | 37  | 37 | 37  | 37 | 37  | 37 | 37  | 62  |
| 10 | 10 | 46 | 46  | 46 | 46  | 46 | 46  | 46 | 46  | 46 | 46  | 46 | 46  | 46 | 46  | 46 | 46  | 77  |
| 11 | 10 | 52 | 52  | 52 | 52  | 52 | 52  | 52 | 52  | 52 | 52  | 52 | 52  | 52 | 52  | 52 | 52  | 88  |
| 12 | 10 | 56 | 56  | 56 | 56  | 56 | 56  | 56 | 56  | 56 | 56  | 56 | 56  | 56 | 56  | 56 | 56  | 93  |
| 13 | 10 | 56 | 56  | 56 | 56  | 56 | 56  | 56 | 56  | 56 | 56  | 56 | 56  | 56 | 56  | 56 | 56  | 94  |
| 14 | 9  | 64 | 64  | 64 | 64  | 64 | 64  | 75 | 85  | 92 | 94  | 92 | 85  | 76 | 64  | 64 | 64  | 128 |
| 15 | 9  | 57 | 57  | 57 | 57  | 57 | 57  | 62 | 74  | 84 | 89  | 90 | 85  | 77 | 65  | 57 | 57  | 115 |
| 16 | 9  | 48 | 48  | 48 | 48  | 48 | 48  | 48 | 59  | 71 | 79  | 83 | 81  | 74 | 63  | 50 | 48  | 95  |
| 17 | 10 | 29 | 29  | 29 | 29  | 29 | 29  | 29 | 29  | 29 | 29  | 29 | 29  | 29 | 29  | 29 | 29  | 48  |
| 18 | 10 | 16 | 16  | 16 | 16  | 16 | 16  | 16 | 16  | 16 | 16  | 16 | 16  | 16 | 16  | 16 | 16  | 26  |

Table 6.3.2 June 21. Hourly solar radiation on unit surface area [BTU/h/ft<sup>2</sup>]

| TM | CC | N  | NNE | NE  | ENE | E   | ESE | SE  | SSE | S   | SSW | SW  | WSW | W   | WNW | NW | NNW | RF  |
|----|----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|-----|-----|
| 7  | 2  | 37 | 37  | 124 | 200 | 250 | 269 | 252 | 202 | 127 | 38  | 37  | 37  | 37  | 37  | 37 | 37  | 86  |
| 8  | 2  | 47 | 47  | 101 | 182 | 242 | 273 | 269 | 232 | 166 | 83  | 47  | 47  | 47  | 47  | 47 | 47  | 141 |
| 9  | 2  | 57 | 57  | 72  | 152 | 218 | 260 | 270 | 248 | 198 | 125 | 57  | 57  | 57  | 57  | 57 | 57  | 190 |
| 10 | 3  | 72 | 72  | 72  | 116 | 176 | 220 | 242 | 237 | 208 | 158 | 95  | 72  | 72  | 72  | 72 | 72  | 225 |
| 11 | 4  | 84 | 84  | 84  | 87  | 138 | 181 | 209 | 218 | 207 | 177 | 132 | 84  | 84  | 84  | 84 | 84  | 244 |
| 12 | 5  | 91 | 91  | 91  | 91  | 107 | 145 | 175 | 193 | 195 | 181 | 153 | 116 | 91  | 91  | 91 | 91  | 246 |
| 13 | 5  | 94 | 94  | 94  | 94  | 94  | 121 | 157 | 183 | 196 | 194 | 176 | 146 | 108 | 94  | 94 | 94  | 255 |
| 14 | 5  | 94 | 94  | 94  | 94  | 94  | 94  | 134 | 169 | 192 | 200 | 193 | 170 | 136 | 95  | 94 | 94  | 255 |
| 15 | 5  | 91 | 91  | 91  | 91  | 91  | 91  | 107 | 149 | 182 | 201 | 203 | 189 | 159 | 119 | 91 | 91  | 246 |
| 16 | 6  | 82 | 82  | 82  | 82  | 82  | 82  | 82  | 114 | 147 | 170 | 180 | 174 | 155 | 125 | 88 | 82  | 206 |
| 17 | 7  | 67 | 67  | 67  | 67  | 67  | 67  | 67  | 80  | 109 | 131 | 144 | 145 | 134 | 113 | 85 | 67  | 157 |
| 18 | 8  | 49 | 49  | 49  | 49  | 49  | 49  | 49  | 50  | 71  | 88  | 100 | 103 | 99  | 87  | 69 | 49  | 106 |
| 19 | 9  | 30 | 30  | 30  | 30  | 30  | 30  | 30  | 30  | 37  | 46  | 53  | 57  | 56  | 51  | 43 | 33  | 58  |
| 20 | 9  | 19 | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 23  | 32  | 40  | 44  | 44  | 41  | 35 | 26  | 36  |

Table 6.3.3 September 21. Houlry solar radiation on unit surface area [BTU/h/ft<sup>2</sup>]

| TM | CC | N  | NNE | NE  | ENE | E   | ESE | SE  | SSE | S   | SSW | SW  | WSW | W   | WNW | NW  | NNW | RF  |
|----|----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 8  | 0  | 27 | 27  | 105 | 222 | 310 | 354 | 349 | 295 | 200 | 78  | 27  | 27  | 27  | 27  | 27  | 27  | 82  |
| 9  | 0  | 33 | 33  | 54  | 171 | 267 | 328 | 343 | 312 | 237 | 132 | 33  | 33  | 33  | 33  | 33  | 33  | 144 |
| 10 | 0  | 37 | 37  | 37  | 111 | 212 | 286 | 323 | 315 | 266 | 182 | 75  | 37  | 37  | 37  | 37  | 37  | 195 |
| 11 | 0  | 41 | 41  | 41  | 47  | 149 | 234 | 290 | 307 | 285 | 225 | 137 | 41  | 41  | 41  | 41  | 41  | 234 |
| 12 | 0  | 43 | 43  | 43  | 43  | 81  | 173 | 247 | 289 | 293 | 260 | 193 | 104 | 43  | 43  | 43  | 43  | 260 |
| 13 | 0  | 44 | 44  | 44  | 44  | 44  | 108 | 196 | 261 | 293 | 286 | 243 | 170 | 77  | 44  | 44  | 44  | 271 |
| 14 | 0  | 44 | 44  | 44  | 44  | 44  | 44  | 141 | 225 | 282 | 303 | 284 | 229 | 145 | 46  | 44  | 44  | 270 |
| 15 | 0  | 42 | 42  | 42  | 42  | 42  | 42  | 82  | 184 | 263 | 310 | 315 | 279 | 207 | 110 | 42  | 42  | 254 |
| 16 | 0  | 40 | 40  | 40  | 40  | 40  | 40  | 137 | 236 | 305 | 334 | 318 | 260 | 168 | 57  | 40  | 225 | 183 |
| 17 | 0  | 36 | 36  | 36  | 36  | 36  | 36  | 36  | 87  | 201 | 289 | 339 | 343 | 300 | 217 | 107 | 36  | 183 |
| 18 | 0  | 31 | 31  | 31  | 31  | 31  | 31  | 31  | 36  | 158 | 261 | 329 | 351 | 325 | 254 | 150 | 31  | 129 |
| 19 | 0  | 26 | 26  | 26  | 26  | 26  | 26  | 26  | 26  | 111 | 221 | 302 | 341 | 331 | 275 | 182 | 64  | 65  |

Table 6.3.4 December 21. Houlry solar radiation on unit surface area [BTU/h/ft<sup>2</sup>]

| TM | CC | N  | NNE | NE | ENE | E  | ESE | SE | SSE | S  | SSW | SW | WSW | W  | WNW | NW | NNW | RF |
|----|----|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|----|
| 8  | 10 | 10 | 10  | 10 | 10  | 10 | 10  | 10 | 10  | 10 | 10  | 10 | 10  | 10 | 10  | 10 | 10  | 16 |
| 9  | 10 | 22 | 22  | 22 | 22  | 22 | 22  | 22 | 22  | 22 | 22  | 22 | 22  | 22 | 22  | 22 | 22  | 37 |
| 10 | 10 | 31 | 31  | 31 | 31  | 31 | 31  | 31 | 31  | 31 | 31  | 31 | 31  | 31 | 31  | 31 | 31  | 53 |
| 11 | 10 | 38 | 38  | 38 | 38  | 38 | 38  | 38 | 38  | 38 | 38  | 38 | 38  | 38 | 38  | 38 | 38  | 63 |
| 12 | 10 | 41 | 41  | 41 | 41  | 41 | 41  | 41 | 41  | 41 | 41  | 41 | 41  | 41 | 41  | 41 | 41  | 69 |
| 13 | 10 | 41 | 41  | 41 | 41  | 41 | 41  | 41 | 41  | 41 | 41  | 41 | 41  | 41 | 41  | 41 | 41  | 68 |
| 14 | 10 | 37 | 37  | 37 | 37  | 37 | 37  | 37 | 37  | 37 | 37  | 37 | 37  | 37 | 37  | 37 | 37  | 62 |
| 15 | 10 | 31 | 31  | 31 | 31  | 31 | 31  | 31 | 31  | 31 | 31  | 31 | 31  | 31 | 31  | 31 | 31  | 51 |
| 16 | 10 | 21 | 21  | 21 | 21  | 21 | 21  | 21 | 21  | 21 | 21  | 21 | 21  | 21 | 21  | 21 | 21  | 35 |
| 17 | 10 | 9  | 9   | 9  | 9   | 9  | 9   | 9  | 9   | 9  | 9   | 9  | 9   | 9  | 9   | 9  | 9   | 14 |

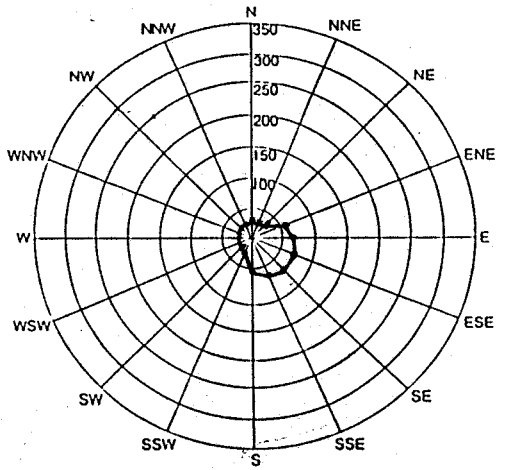


Fig. 6.1.1 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], March 21, 8:00 a.m., Cloud cover = 9

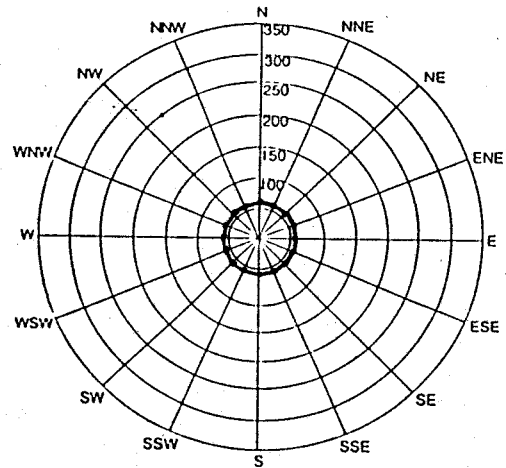


Fig. 6.1.2 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], March 21, 12:00 noon, Cloud cover = 10

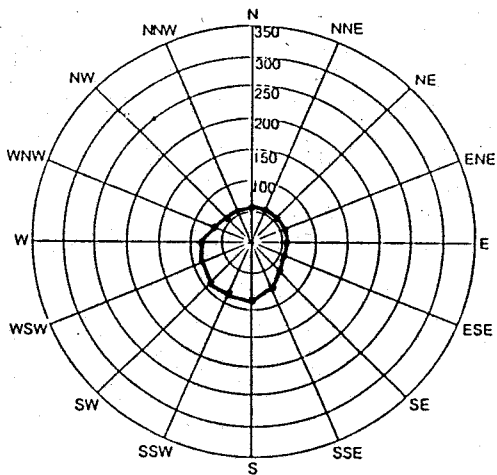


Fig. 6.1.3 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], March 21, 3:00 p.m., Cloud cover = 9

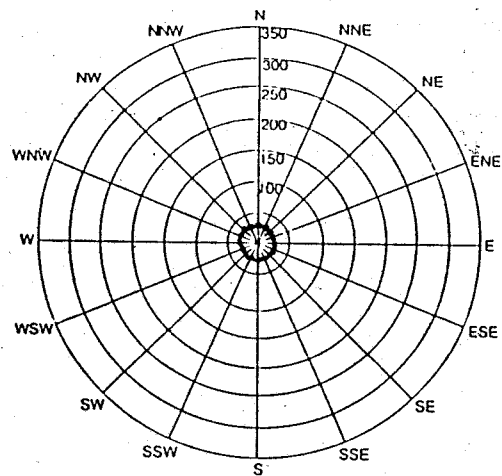


Fig. 6.1.4 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], March 21, 5:00 p.m., Cloud cover = 10



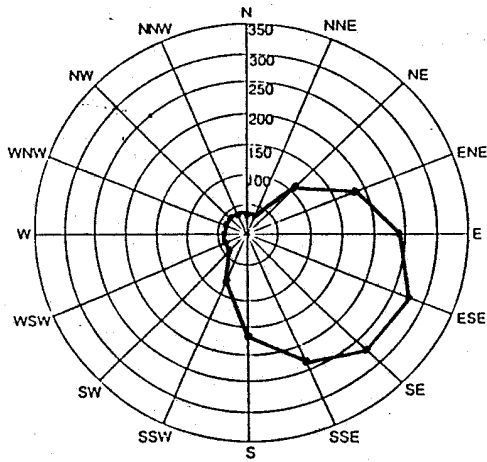


Fig. 6.2.1 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], June 21, 8:00 a.m., Cloud cover = 2

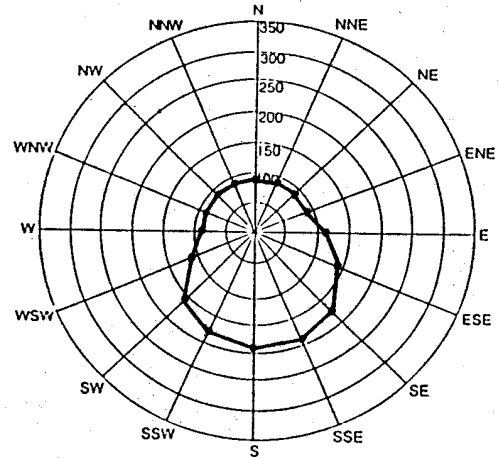


Fig. 6.2.2 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], June 21, 12:00 noon, Cloud cover = 5

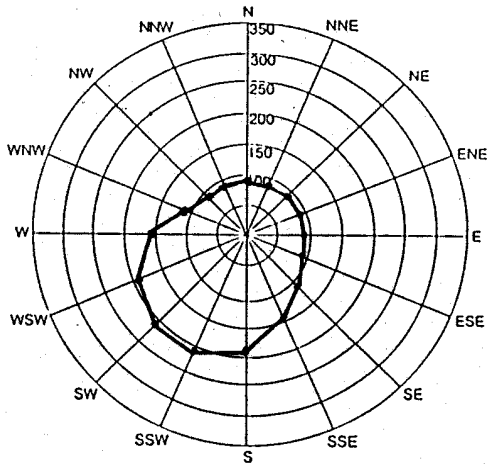


Fig. 6.2.3 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], June 21, 3:00 p.m., Cloud cover = 5

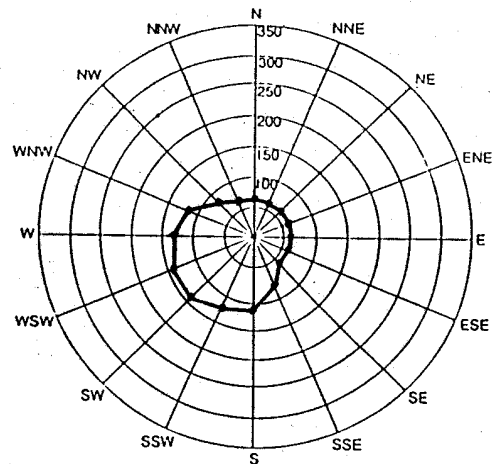


Fig. 6.2.4 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], June 21, 5:00 p.m., Cloud cover = 7

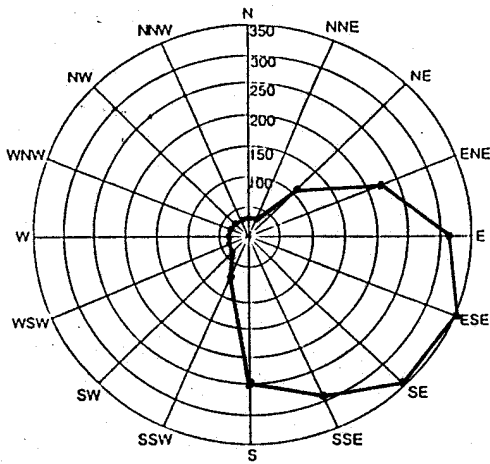


Fig. 6.3.1 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], September 21, 8:00 a.m., Cloud cover = 0

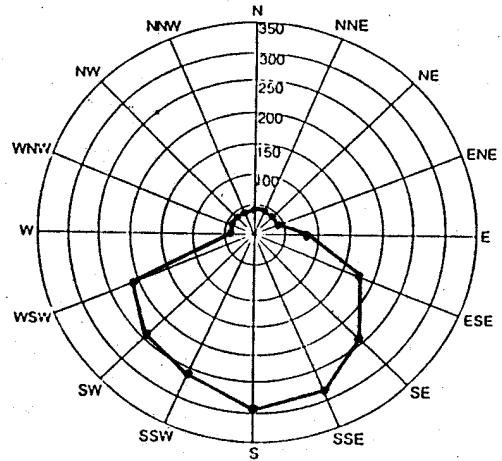


Fig. 6.3.2 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], September 21, 12:00 noon, Cloud cover = 0

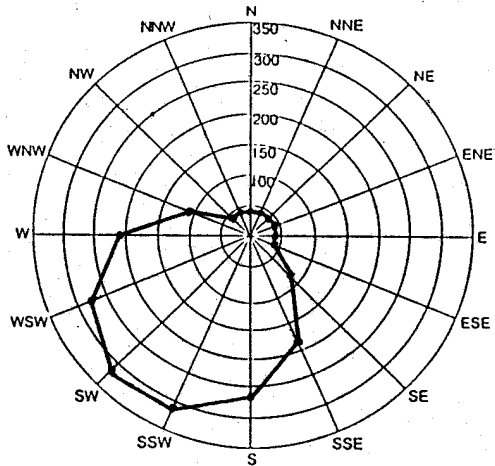


Fig. 6.3.3 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], September 21, 3:00 p.m., Cloud cover = 0

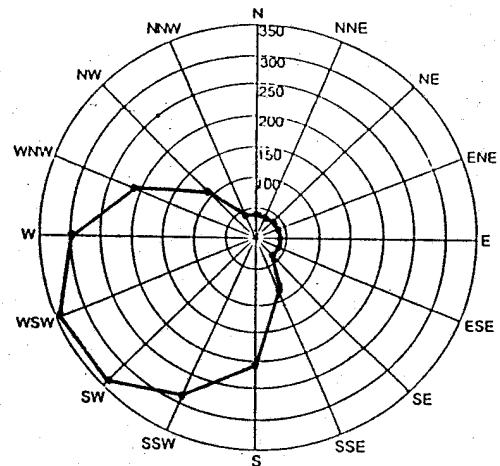


Fig. 6.3.4 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], September 21, 5:00 p.m., Cloud cover = 0

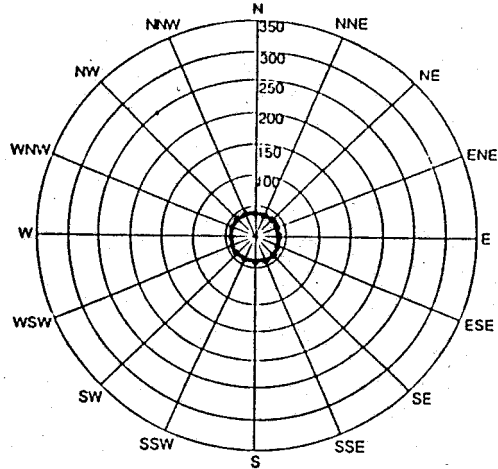


Fig. 6.4 Solar radiation on unit surface area [BTU/h/ft<sup>2</sup>], December 21, 12:00 noon, Cloud cover = 10

Among the averages of daily sum values, those of December, January, and February were selected for winter heat loss amount calculations and those of June, July and August were selected for summer heat gain amount calculations for the 41 different building shapes and 16 different orientations. Tables 6.4 and 6.5 give the averages of daily total heat flow amounts through the unit surface area of the walls in summer and winter. And the values were plotted as shown in figures 6.5.1 and 6.5.2.

Table 6.4 Average of daily total heat gain through unit surface area in summer [Btu/day/ft<sup>2</sup>]

| Mo\Or | N  | NNE | NE | ENE | E  | ESE | SE | SSE | S  | SSW | SW | WSW | W  | WNW | NW | NNW | Roof |
|-------|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|------|
| Jun.  | 21 | 23  | 25 | 27  | 27 | 26  | 24 | 21  | 20 | 22  | 25 | 27  | 28 | 28  | 26 | 23  | 26   |
| Jul.  | 38 | 40  | 44 | 47  | 48 | 47  | 43 | 38  | 36 | 38  | 44 | 47  | 49 | 48  | 45 | 40  | 43   |
| Aug.  | 35 | 37  | 41 | 44  | 45 | 45  | 44 | 41  | 39 | 41  | 44 | 46  | 47 | 45  | 42 | 38  | 38   |
| Ave.  | 31 | 33  | 37 | 39  | 40 | 39  | 37 | 33  | 32 | 34  | 38 | 40  | 41 | 40  | 38 | 34  | 36   |

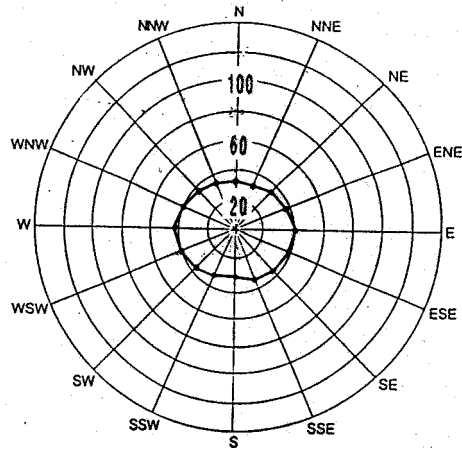


Fig. 6.5.1 Summer heat gain through unit surface area [BTU/day/ft<sup>2</sup>]

Table 6.5 Average of daily total heat loss through unit surface area in winter [Btu/day/ft<sup>2</sup>]

| Mo\Or | N   | NNE | NE  | ENE | E   | ESE | SE  | SSE | S   | SSW | SW  | WSW | W   | WNW | NW  | NNW | Roof |
|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
| Dec.  | -86 | -86 | -85 | -81 | -77 | -72 | -68 | -65 | -63 | -65 | -68 | -72 | -76 | -81 | -84 | -86 | -91  |
| Jan.  | -99 | -99 | -98 | -95 | -92 | -88 | -84 | -81 | -79 | -81 | -84 | -88 | -91 | -95 | -98 | -99 | -105 |
| Feb.  | -90 | -90 | -89 | -86 | -83 | -80 | -78 | -76 | -75 | -75 | -76 | -78 | -81 | -85 | -88 | -90 | -95  |
| Ave.  | -92 | -92 | -91 | -87 | -84 | -80 | -77 | -74 | -72 | -74 | -76 | -79 | -83 | -87 | -90 | -92 | -97  |

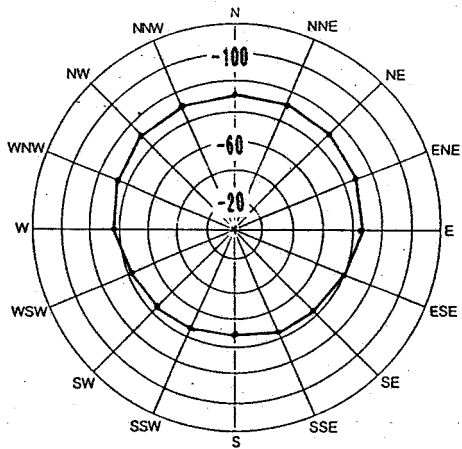


Fig. 6.5.2 Winter heat loss through unit surface area [BTU/day/ft<sup>2</sup>]

As shown in the figures 6.4 and 6.5, winter heat loss is greater than summer heat gain in Oklahoma City area. In summer, east and west walls passed more heat into the building than north and south walls. This indicates that the low altitude angles of the early morning and late afternoon sun in summer season caused greater direct solar radiation intensities on the east and west walls. In winter, differently from the summer case, north wall caused greatest heat loss due to no direct solar radiation on the wall in this season.

Table 6.6 shows an example of the average of daily total heat gain and loss for 12 calendar months in the building which had the width-to-length ratio of 1:1 and the front wall azimuth angle of 0° south.

**Table 6.6 An example of average of daily total heat gain and loss in each month**

| BLDG ORIENTATION = South<br>WIDTH : LENGTH = 1 : 1 |                |               |
|--|----------------|---------------|
| Month  | HEAT LOSS      | HEAT GAIN     |
| 1  | <u>-305590</u> | 32759         |
| 2  | <u>-266966</u> | 24552         |
| 3  | -126485        | 68172         |
| 4  | -66808         | 98527         |
| 5  | -55325         | 103249        |
| 6  | -10592         | <u>195309</u> |
| 7  | -1711          | <u>278446</u> |
| 8  | -4100          | <u>259641</u> |
| 9  | -21186         | 180001        |
| 10   | -90613         | 100379        |
| 11   | -160223        | 75922         |
| 12   | <u>-258292</u> | 50107         |
| SUMMER GAIN : 244465 (BTU/day)                     |                |               |
| WINTER LOSS : -276950 (BTU/day)                    |                |               |

### 6.3 The Output Data of the Simulations

The final output data sets were obtained by tabulating the summer heat gain and winter heat loss values (BTU/day) for entire 41 building shapes as shown in tables 6.7.1 and 6.7.2. These tables show, as an example, the daily average heat gain and heat loss in the buildings having south orientation. As in Olgyay's work (Olgyay, Victor, 1963, p. 88), the values of heat gain and loss in square house were considered as starting reference points, and therefore set to zero. The heat gain or heat loss amounts in other forms were linearly transformed by subtracting the square building's heat gain and loss amounts.

**Table 6.7.1 Final output data set for winter  
heat loss and summer heat gain [BTU/Day],  
Orientation 0°S**

| W : L     | Winter  | Summer | Loss   | Gain  |
|-----------|---------|--------|--------|-------|
| 5.0 : 1.0 | -306651 | 254531 | -29701 | 10066 |
| 4.5 : 1.0 | -303290 | 252916 | -26340 | 8451  |
| 4.0 : 1.0 | -299113 | 251286 | -22163 | 6821  |
| 3.5 : 1.0 | -294869 | 249652 | -17919 | 5187  |
| 3.0 : 1.0 | -290578 | 248041 | -13628 | 3576  |
| 2.5 : 1.0 | -286305 | 246505 | -9355  | 2040  |
| 2.4 : 1.0 | -285464 | 246214 | -8514  | 1749  |
| 2.3 : 1.0 | -284631 | 245931 | -7681  | 1466  |
| 2.2 : 1.0 | -283809 | 245658 | -6859  | 1193  |
| 2.1 : 1.0 | -283001 | 245396 | -6051  | 931   |
| 2.0 : 1.0 | -282210 | 245147 | -5260  | 682   |
| 1.9 : 1.0 | -281439 | 244915 | -4489  | 450   |
| 1.8 : 1.0 | -280696 | 244702 | -3746  | 237   |
| 1.7 : 1.0 | -279985 | 244512 | -3035  | 47    |
| 1.6 : 1.0 | -279314 | 244350 | -2364  | -115  |
| 1.5 : 1.0 | -278692 | 244222 | -1742  | -243  |
| 1.4 : 1.0 | -278133 | 244136 | -1183  | -329  |
| 1.3 : 1.0 | -277653 | 244102 | -703   | -363  |
| 1.2 : 1.0 | -277274 | 244133 | -324   | -332  |
| 1.1 : 1.0 | -277026 | 244246 | -76    | -219  |
| 1.0 : 1.0 | -276950 | 244465 | 0      | 0     |

**Table 6.7.2 Final output data set for winter  
heat loss and summer heat gain [BTU/day],  
Orientation 0°S**

| W : L     | Winter  | Summer | Loss   | Gain  |
|-----------|---------|--------|--------|-------|
| 1.0 : 1.1 | -277076 | 244785 | -126   | 320   |
| 1.0 : 1.2 | -277370 | 245166 | -420   | 701   |
| 1.0 : 1.3 | -277791 | 245591 | -841   | 1126  |
| 1.0 : 1.4 | -278310 | 246049 | -1360  | 1584  |
| 1.0 : 1.5 | -278906 | 246533 | -1956  | 2068  |
| 1.0 : 1.6 | -279562 | 247035 | -2612  | 2570  |
| 1.0 : 1.7 | -280266 | 247551 | -3316  | 3086  |
| 1.0 : 1.8 | -281009 | 248078 | -4059  | 3613  |
| 1.0 : 1.9 | -281781 | 248613 | -4831  | 4148  |
| 1.0 : 2.0 | -282578 | 249153 | -5628  | 4688  |
| 1.0 : 2.1 | -283396 | 249697 | -6446  | 5232  |
| 1.0 : 2.2 | -284230 | 250244 | -7280  | 5779  |
| 1.0 : 2.3 | -285077 | 250792 | -8127  | 6327  |
| 1.0 : 2.4 | -285934 | 251339 | -8984  | 6874  |
| 1.0 : 2.5 | -286799 | 251887 | -9849  | 7422  |
| 1.0 : 3.0 | -291180 | 254600 | -14230 | 10135 |
| 1.0 : 3.5 | -295568 | 257250 | -18618 | 12785 |
| 1.0 : 4.0 | -299905 | 259821 | -22955 | 15356 |
| 1.0 : 4.5 | -304166 | 262313 | -27216 | 17848 |
| 1.0 : 5.0 | -308337 | 264728 | -31387 | 20263 |

## **6.4 Interpretation of the Output Data**

The output data sets of same formats shown in the tables 6.7.1 and 6.7.2 were plotted for 16 different orientations. Then, from the tables and figures the optimum building shapes for 16 different orientations in the Oklahoma City area were identified.

An optimum building shape for each season, summer or winter, was identified from the tables, then, an optimum shape concerning both seasons was suggested by examining the heat gain and heat loss patterns of the figures.

### **6.4.1 Optimum Building Shape for South Orientation**

As indicated in table 6.8 and figure 6.6, the minimum summer heat gain was yielded by the building having width-to-length ratio of 1.3:1.0. In winter, however, the square building produced minimum heat loss.

For a building oriented toward the south, the width-to-length ratios between 1:1 and 1.3:1 which should be elongated along the east and west axis might be suggested as the optimum shapes. Any shape between these width-to-length ratios might produce not far more heat loss in winter and less heat gain in summer than the square form.

Since the buildings of any other width-to-length ratios produced greater heat loss in winter, which has dominant impact on building energy requirements in the Oklahoma City area, any more elongation along the east and west axis or any elongation along the south and north axis might not be desirable.



Table 6.8 Daily average heat gain and heat loss in buildings oriented to the south [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -205168     | 80841       | -3362      | -84        |
| 1.5 : 1.0 | -204452     | 80705       | -2646      | -220       |
| 1.4 : 1.0 | -203811     | 80611       | -2005      | -314       |
| 1.3 : 1.0 | -203263     | 80570       | -1457      | -355       |
| 1.2 : 1.0 | -202834     | 80596       | -1028      | -329       |
| 1.1 : 1.0 | -202559     | 80706       | -753       | -219       |
| 1.0 : 1.0 | -201806     | 80925       | 0          | 0          |
| 1.0 : 1.1 | -202654     | 81247       | -95        | 322        |
| 1.0 : 1.2 | -203014     | 81633       | -455       | 708        |
| 1.0 : 1.3 | -203523     | 82064       | -964       | 1139       |
| 1.0 : 1.4 | -204145     | 82531       | -1586      | 1606       |
| 1.0 : 1.5 | -204856     | 83023       | -2297      | 2098       |
| 1.0 : 1.6 | -205637     | 83536       | -3078      | 2611       |

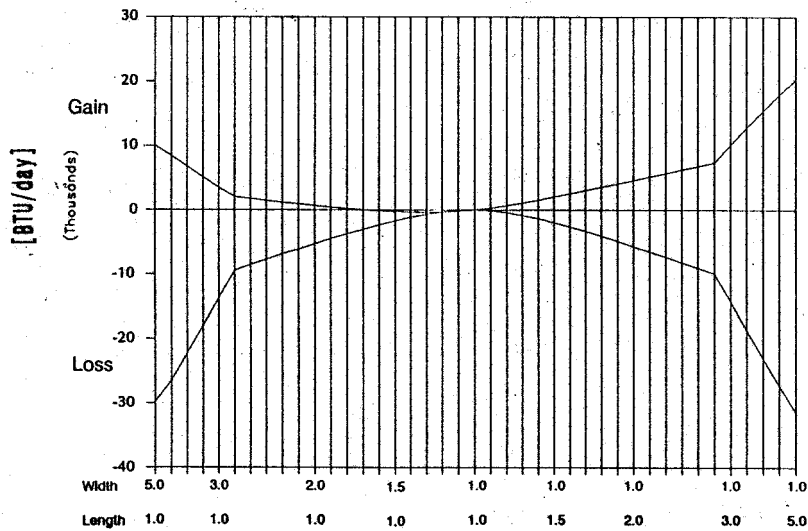


Fig. 6.6 Daily average heat gain and heat loss for the south orientation

#### **6.4.2 Optimum Building Shape for North Orientation**

As shown in table 6.9 and figure 6.7, for a building oriented toward the north, the width-to-length ratios between 1:1 and 1.3:1 which should be elongated along the east and west axis might be suggested as the optimum shapes.

#### **6.4.3 Optimum Building Shape for East Orientation**

As indicated in table 6.10 and figure 6.8, for a building oriented toward the east, the width-to-length ratios between 1:1 and 1:1.3 which should be elongated along the east and west axis might be suggested as the optimum shapes.

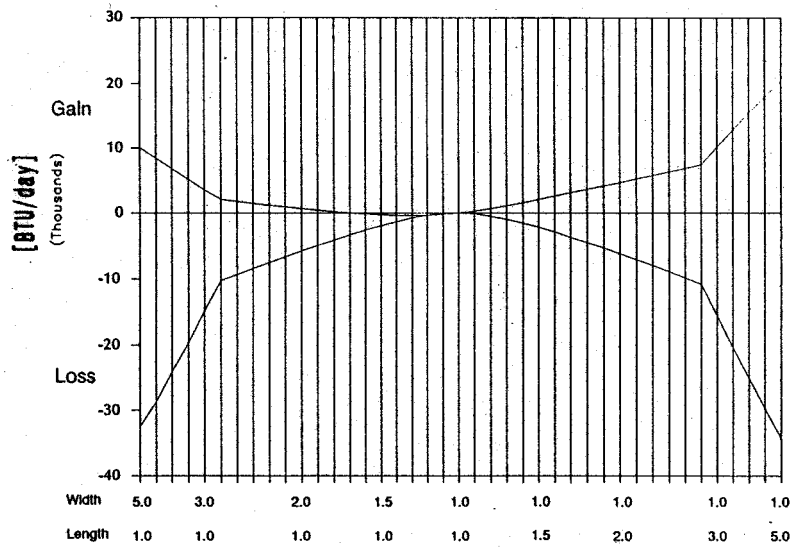
#### **6.4.4 Optimum Building Shape for West Orientation**

As indicated in table 6.11 and figure 6.9, for a building oriented toward the west, the width-to-length ratios between 1:1 and 1:1.3 which should be elongated along the east and west axis might be suggested as the optimum shapes.

After all, for the buildings oriented toward above 4 orientations, the optimum width-to-length ratios were between 1:1 and 1:1.3 or between 1:1 and 1.3:1 elongated along the east and west axis.

**Table 6.9 Daily average heat gain and heat loss in buildings oriented to the north [BTU/day]**

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -290702     | 245043      | -2573      | -115       |
| 1.5 : 1.0 | -290025     | 244915      | -1896      | -243       |
| 1.4 : 1.0 | -289416     | 244829      | -1287      | -329       |
| 1.3 : 1.0 | -288894     | 244794      | -765       | -364       |
| 1.2 : 1.0 | -288481     | 244825      | -352       | -333       |
| 1.1 : 1.0 | -288212     | 244938      | -83        | -220       |
| 1.0 : 1.0 | -288129     | 245158      | 0          | 0          |
| 1.0 : 1.1 | -288268     | 245478      | -139       | 320        |
| 1.0 : 1.2 | -288589     | 245858      | -460       | 700        |
| 1.0 : 1.3 | -289048     | 246283      | -919       | 1125       |
| 1.0 : 1.4 | -289615     | 246742      | -1486      | 1584       |
| 1.0 : 1.5 | -290265     | 247225      | -2136      | 2067       |
| 1.0 : 1.6 | -290981     | 247727      | -2852      | 2569       |



**Fig. 6.7 Daily average heat gain and heat loss for the north orientation**

Table 6.10 Daily average heat gain and heat loss in buildings oriented to the east [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -284056     | 263014      | -2749      | 2570       |
| 1.5 : 1.0 | -283368     | 262512      | -2061      | 2068       |
| 1.4 : 1.0 | -282743     | 262028      | -1436      | 1584       |
| 1.3 : 1.0 | -282197     | 261570      | -890       | 1126       |
| 1.2 : 1.0 | -281754     | 261145      | -447       | 701        |
| 1.1 : 1.0 | -281443     | 260764      | -136       | 320        |
| 1.0 : 1.0 | -281307     | 260444      | 0          | 0          |
| 1.0 : 1.1 | -281384     | 260225      | -77        | -219       |
| 1.0 : 1.2 | -281639     | 260112      | -332       | -332       |
| 1.0 : 1.3 | -282031     | 260081      | -724       | -363       |
| 1.0 : 1.4 | -282529     | 260115      | -1222      | -329       |
| 1.0 : 1.5 | -283110     | 260201      | -1803      | -243       |
| 1.0 : 1.6 | -283756     | 260329      | -2449      | -115       |

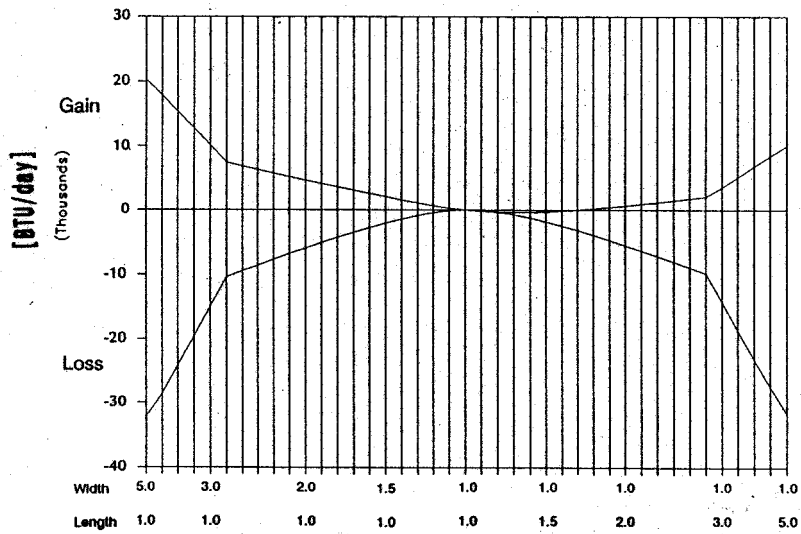
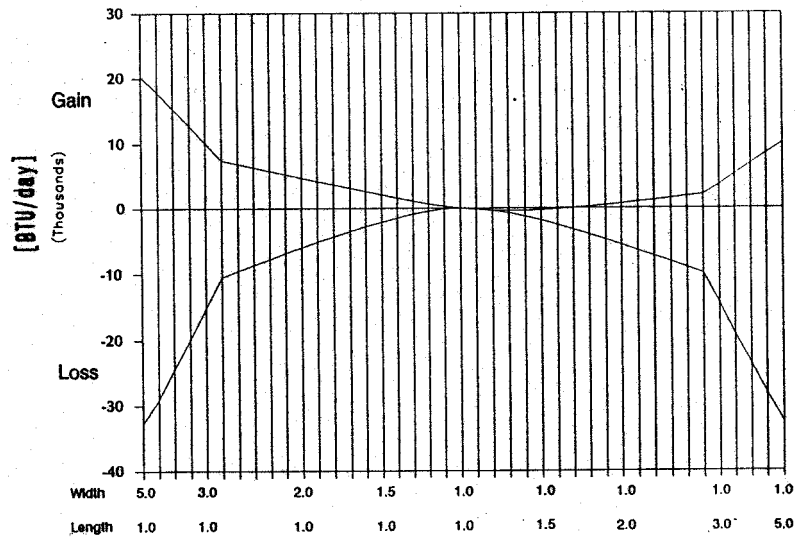


Fig. 6.8 Daily average heat gain and heat loss for the east orientation

**Table 6.11 Daily average heat gain and heat loss  
in buildings oriented to the west [BTU/day]**

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -288207     | 265118      | -2770      | 2568       |
| 1.5 : 1.0 | -287509     | 264616      | -2072      | 2066       |
| 1.4 : 1.0 | -286876     | 264133      | -1439      | 1583       |
| 1.3 : 1.0 | -286325     | 263675      | -888       | 1125       |
| 1.2 : 1.0 | -285880     | 263250      | -443       | 700        |
| 1.1 : 1.0 | -285569     | 262870      | -132       | 320        |
| 1.0 : 1.0 | -285437     | 262550      | 0          | 0          |
| 1.0 : 1.1 | -285522     | 262331      | -85        | -219       |
| 1.0 : 1.2 | -285789     | 262218      | -352       | -332       |
| 1.0 : 1.3 | -286195     | 262187      | -758       | -363       |
| 1.0 : 1.4 | -286710     | 262221      | -1273      | -329       |
| 1.0 : 1.5 | -287308     | 262307      | -1871      | -243       |
| 1.0 : 1.6 | -287973     | 262435      | -2536      | -115       |



**Fig. 6.9 Daily average heat gain and  
heat loss for the west orientation**

#### **6.4.5 Optimum Building Shapes for SE, SW, NE and NW Orientations**

As shown in tables 6.12 through 6.15 and figures 6.10 through 6.13, both minimum summer heat gains and winter loss were yielded by the buildings of square forms.

#### **6.4.6 Optimum Building Shapes for SSE, SSW, ESE and WSW Orientations**

As shown in tables 6.16 through 6.19 and figures 6.14 through 6.17, the minimum summer heat gains were shown at width-to-length ratios of 1.2:1 for SSE and SSW orientations and 1:1.2 for ESE and WSW orientations. In winter, however, the square building yielded the minimum heat loss.

Considering that the differences between the heat gains in square buildings and 1.2:1.0 shaped buildings are minimal, a square building shape is recommended for these orientations.

#### **6.4.7 Optimum Building Shapes for NNE, NNW, ENE and WNW Orientations**

As shown in tables 6.20 through 6.23 and figures 6.18 through 6.21, the minimum summer heat gains were shown at width-to-length ratios of 1.2:1.0 for NNE and NNW orientations and 1.0:1.2 for ENE and WNW orientations. In winter, however, the square building had minimum heat loss. Considering that the differences between the heat gains in square buildings and 1.2:1.0 shaped buildings are minimal, a square building shape is recommended for these orientations.

Table 6.12 Daily average heat gain and heat loss in buildings oriented to the SE [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -206426     | 83589       | -3671      | 1319       |
| 1.5 : 1.0 | -205665     | 83253       | -2910      | 983        |
| 1.4 : 1.0 | -204975     | 82949       | -2220      | 679        |
| 1.3 : 1.0 | -204377     | 82685       | -1622      | 415        |
| 1.2 : 1.0 | -203896     | 82472       | -1141      | 202        |
| 1.1 : 1.0 | -203567     | 82327       | -812       | 57         |
| 1.0 : 1.0 | -202755     | 82270       | 0          | 0          |
| 1.0 : 1.1 | -203549     | 82320       | -794       | 50         |
| 1.0 : 1.2 | -203860     | 82458       | -1105      | 188        |
| 1.0 : 1.3 | -204325     | 82664       | -1570      | 394        |
| 1.0 : 1.4 | -204908     | 82922       | -2153      | 652        |
| 1.0 : 1.5 | -205584     | 83221       | -2829      | 951        |
| 1.0 : 1.6 | -206332     | 83552       | -3577      | 1282       |

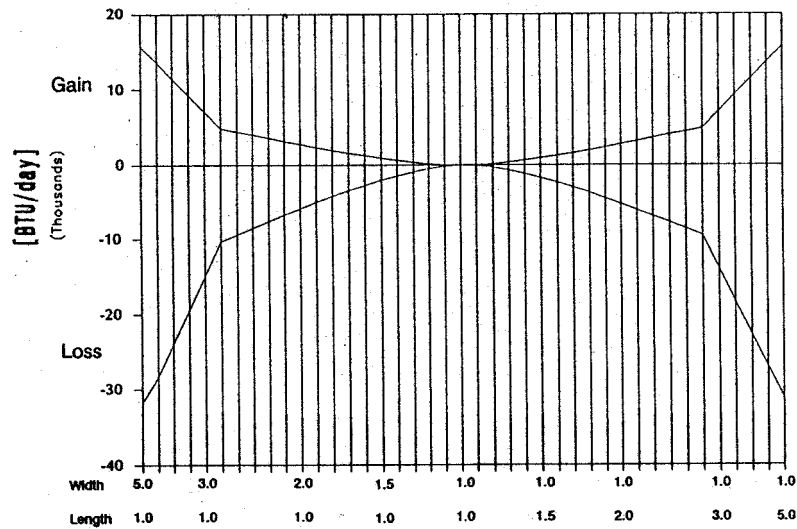
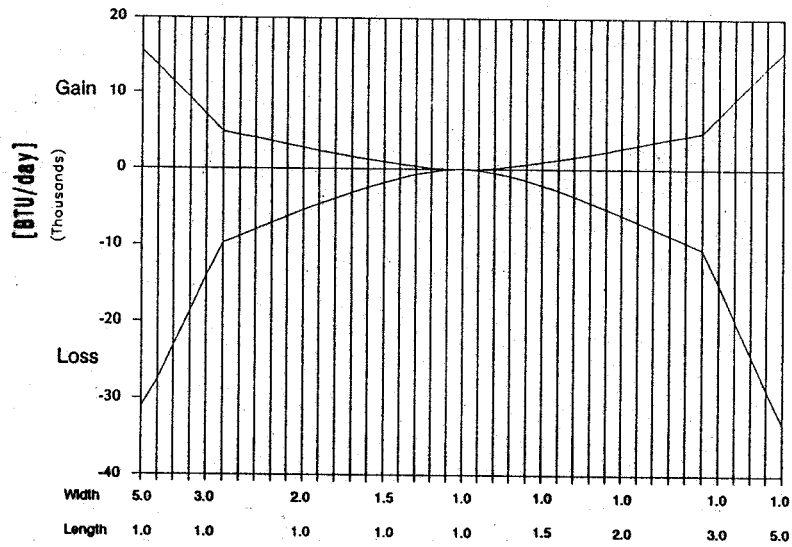


Fig. 6.10 Daily average heat gain and heat loss for the SE orientation

**Table 6.13 Daily average heat gain and heat loss in buildings oriented to the SW [BTU/day]**

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -287942     | 264965      | -2419      | 1265       |
| 1.5 : 1.0 | -287298     | 264640      | -1775      | 940        |
| 1.4 : 1.0 | -286720     | 264347      | -1197      | 647        |
| 1.3 : 1.0 | -286226     | 264093      | -703       | 393        |
| 1.2 : 1.0 | -285839     | 263890      | -316       | 190        |
| 1.1 : 1.0 | -285590     | 263752      | -67        | 52         |
| 1.0 : 1.0 | -285523     | 263700      | 0          | 0          |
| 1.0 : 1.1 | -285670     | 263752      | -147       | 52         |
| 1.0 : 1.2 | -285992     | 263889      | -469       | 189        |
| 1.0 : 1.3 | -286446     | 264092      | -923       | 392        |
| 1.0 : 1.4 | -287003     | 264346      | -1480      | 646        |
| 1.0 : 1.5 | -287640     | 264639      | -2117      | 939        |
| 1.0 : 1.6 | -288339     | 264964      | -2816      | 1264       |

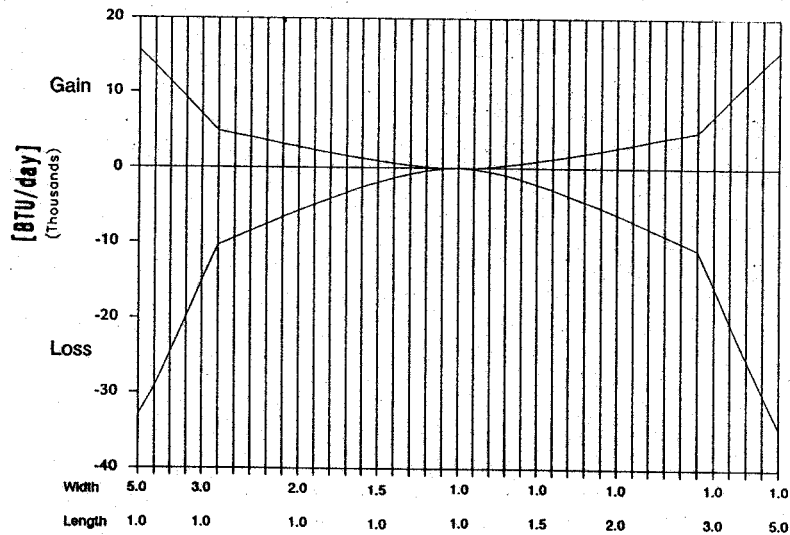


**Fig. 6.11 Daily average heat gain and heat loss for the SW orientation**



**Table 6.14 Daily average heat gain and heat loss  
in buildings oriented to the NE [BTU/day]**

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -292536     | 263392      | -2601      | 1265       |
| 1.5 : 1.0 | -291850     | 263067      | -1915      | 940        |
| 1.4 : 1.0 | -291233     | 262774      | -1298      | 647        |
| 1.3 : 1.0 | -290705     | 262520      | -770       | 393        |
| 1.2 : 1.0 | -290289     | 262317      | -354       | 190        |
| 1.1 : 1.0 | -290018     | 262179      | -83        | 52         |
| 1.0 : 1.0 | -289935     | 262127      | 0          | 0          |
| 1.0 : 1.1 | -290078     | 262179      | -143       | 52         |
| 1.0 : 1.2 | -290405     | 262316      | -470       | 189        |
| 1.0 : 1.3 | -290871     | 262519      | -936       | 392        |
| 1.0 : 1.4 | -291446     | 262773      | -1511      | 646        |
| 1.0 : 1.5 | -292106     | 263066      | -2171      | 939        |
| 1.0 : 1.6 | -292832     | 263391      | -2897      | 1264       |



**Fig. 6.12 Daily average heat gain and  
heat loss for the NE orientation**

Table 6.15 Daily average heat gain and heat loss in buildings oriented to the NW [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -294099     | 265090      | -2900      | 1263       |
| 1.5 : 1.0 | -293372     | 264766      | -2173      | 939        |
| 1.4 : 1.0 | -292712     | 264473      | -1513      | 646        |
| 1.3 : 1.0 | -292136     | 264219      | -937       | 392        |
| 1.2 : 1.0 | -291668     | 264016      | -469       | 189        |
| 1.1 : 1.0 | -291341     | 263879      | -142       | 52         |
| 1.0 : 1.0 | -291199     | 263827      | 0          | 0          |
| 1.0 : 1.1 | -291282     | 263879      | -83        | 52         |
| 1.0 : 1.2 | -291554     | 264017      | -355       | 190        |
| 1.0 : 1.3 | -291971     | 264220      | -772       | 393        |
| 1.0 : 1.4 | -292500     | 264474      | -1301      | 647        |
| 1.0 : 1.5 | -293118     | 264767      | -1919      | 940        |
| 1.0 : 1.6 | -293806     | 265091      | -2607      | 1264       |

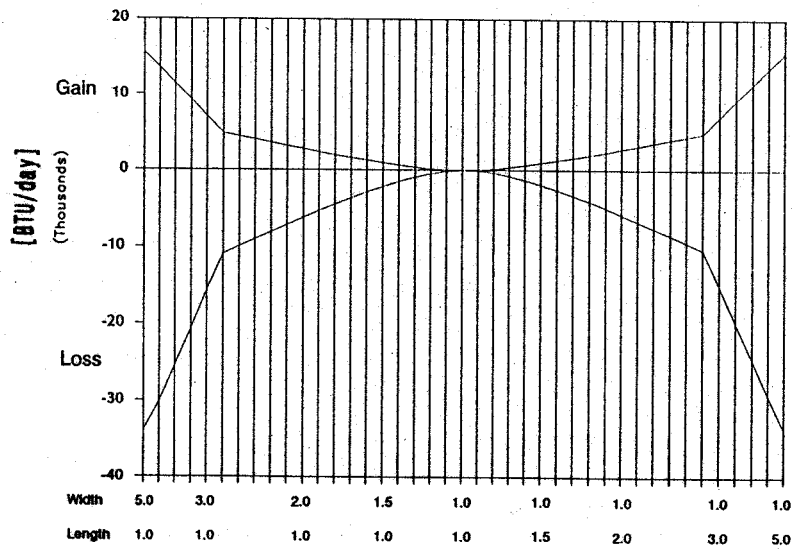


Fig. 6.13 Daily average heat gain and heat loss for the NW orientation

Table 6.16 Daily average heat gain and heat loss in buildings oriented to the SSE [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff.  |
|-----------|-------------|-------------|------------|-------------|
| 1.6 : 1.0 | -280495     | 251949      | -2592      | 330         |
| 1.5 : 1.0 | -279839     | 251757      | -1936      | 138         |
| 1.4 : 1.0 | -279244     | 251603      | -1341      | -16         |
| 1.3 : 1.0 | -278727     | 251498      | -824       | -121        |
| 1.2 : 1.0 | -278310     | 251454      | -407       | <u>-165</u> |
| 1.1 : 1.0 | -278022     | 251486      | -119       | -133        |
| 1.0 : 1.0 | -277903     | 251619      | <u>0</u>   | 0           |
| 1.0 : 1.1 | -277989     | 251854      | -86        | 235         |
| 1.0 : 1.2 | -278247     | 252158      | -344       | 539         |
| 1.0 : 1.3 | -278637     | 252513      | -734       | 894         |
| 1.0 : 1.4 | -279128     | 252907      | -1225      | 1288        |
| 1.0 : 1.5 | -279699     | 253332      | -1796      | 1713        |
| 1.0 : 1.6 | -280334     | 253779      | -2431      | 2160        |

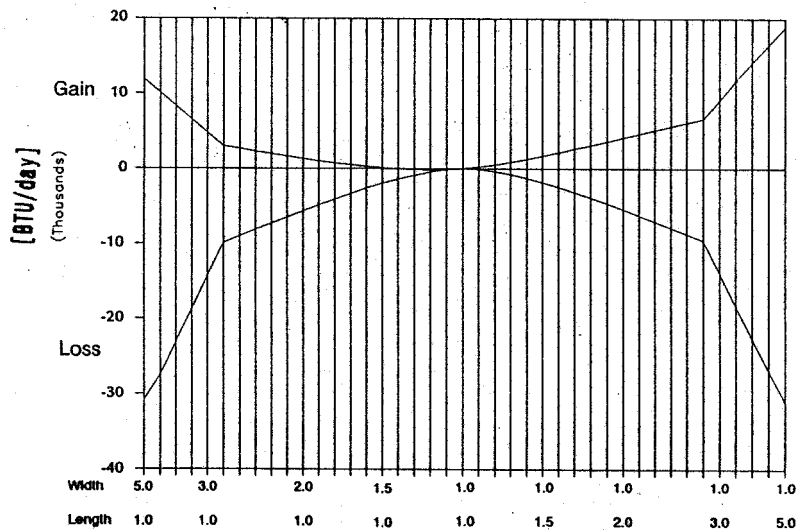


Fig. 6.14 Daily average heat gain and heat loss for the SSE orientation

Table 6.17 Daily average heat gain and heat loss in buildings oriented to the SSW [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff.  |
|-----------|-------------|-------------|------------|-------------|
| 1.6 : 1.0 | -283636     | 252293      | -2324      | 330         |
| 1.5 : 1.0 | -283014     | 252101      | -1702      | 138         |
| 1.4 : 1.0 | -282457     | 251948      | -1145      | -15         |
| 1.3 : 1.0 | -281981     | 251842      | -669       | -121        |
| 1.2 : 1.0 | -281610     | 251798      | -298       | <u>-165</u> |
| 1.1 : 1.0 | -281373     | 251830      | -61        | -133        |
| 1.0 : 1.0 | -281312     | 251963      | <u>0</u>   | 0           |
| 1.0 : 1.1 | -281460     | 252198      | -148       | 235         |
| 1.0 : 1.2 | -281776     | 252501      | -464       | 538         |
| 1.0 : 1.3 | -282220     | 252856      | -908       | 893         |
| 1.0 : 1.4 | -282764     | 253251      | -1452      | 1288        |
| 1.0 : 1.5 | -283385     | 253675      | -2073      | 1712        |
| 1.0 : 1.6 | -284067     | 254121      | -2755      | 2158        |

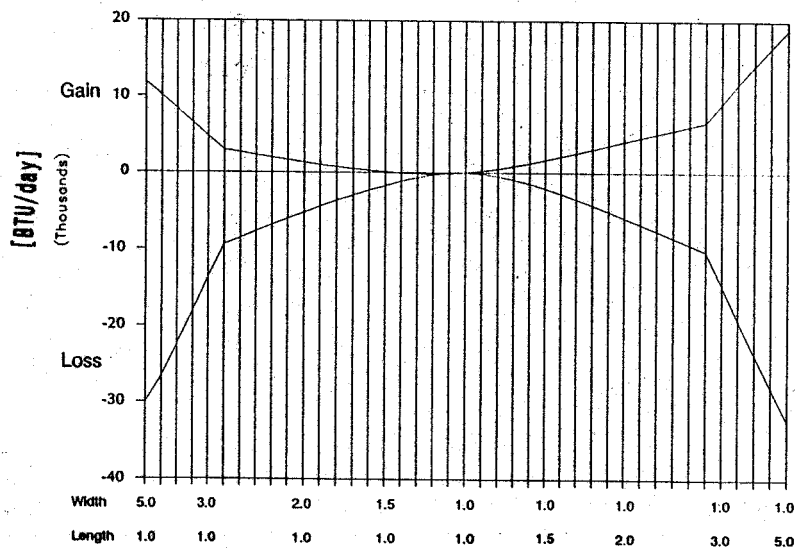


Fig. 6.15 Daily average heat gain and heat loss for the SSW orientation

Table 6.18 Daily average heat gain and heat loss in buildings oriented to the ESE [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -283402     | 264778      | -2793      | 2158       |
| 1.5 : 1.0 | -282711     | 264331      | -2102      | 1711       |
| 1.4 : 1.0 | -282081     | 263907      | -1472      | 1287       |
| 1.3 : 1.0 | -281530     | 263513      | -921       | 893        |
| 1.2 : 1.0 | -281079     | 263158      | -470       | 538        |
| 1.1 : 1.0 | -280758     | 262854      | -149       | 234        |
| 1.0 : 1.0 | -280609     | 262620      | 0          | 0          |
| 1.0 : 1.1 | -280670     | 262487      | -61        | -133       |
| 1.0 : 1.2 | -280910     | 262454      | -301       | -166       |
| 1.0 : 1.3 | -281286     | 262499      | -677       | -121       |
| 1.0 : 1.4 | -281769     | 262604      | -1160      | -16        |
| 1.0 : 1.5 | -282334     | 262758      | -1725      | 138        |
| 1.0 : 1.6 | -282965     | 262950      | -2356      | 330        |

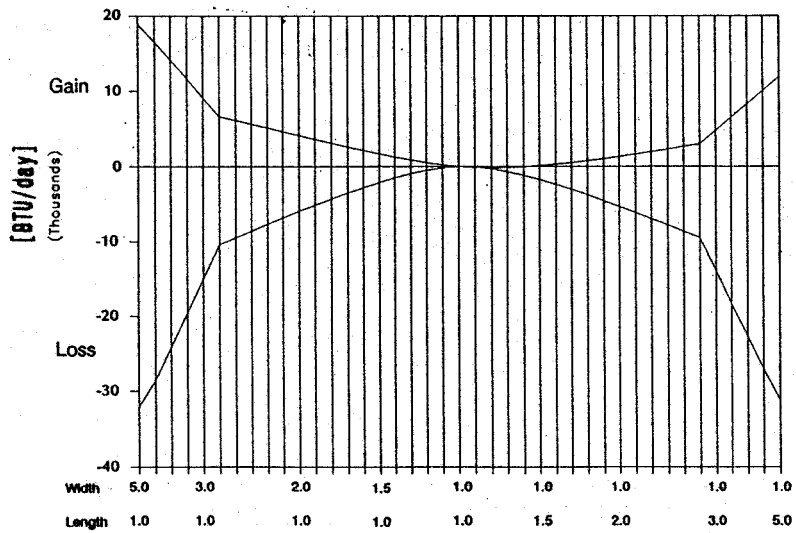


Fig. 6.16 Daily average heat gain and heat loss for the ESE orientation

Table 6.19 Daily average heat gain and heat loss in buildings oriented to the WSW [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -287890     | 266975      | -2573      | 2159       |
| 1.5 : 1.0 | -287220     | 266528      | -1903      | 1712       |
| 1.4 : 1.0 | -286617     | 266104      | -1300      | 1288       |
| 1.3 : 1.0 | -286098     | 265710      | -781       | 894        |
| 1.2 : 1.0 | -285685     | 265354      | -368       | 538        |
| 1.1 : 1.0 | -285410     | 265051      | -93        | 235        |
| 1.0 : 1.0 | -285317     | 264816      | 0          | 0          |
| 1.0 : 1.1 | -285440     | 264683      | -123       | -133       |
| 1.0 : 1.2 | -285742     | 264650      | -425       | -166       |
| 1.0 : 1.3 | -286179     | 264695      | -862       | -121       |
| 1.0 : 1.4 | -286721     | 264800      | -1404      | -16        |
| 1.0 : 1.5 | -287345     | 264954      | -2028      | 138        |
| 1.0 : 1.6 | -288034     | 265145      | -2717      | 329        |

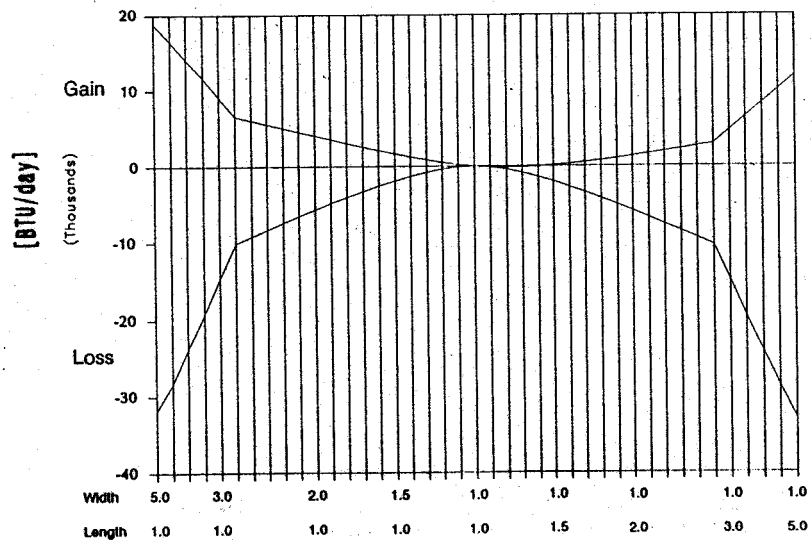


Fig. 6.17 Daily average heat gain and heat loss for the WSW orientation

Table 6.20 Daily average heat gain and heat loss in buildings oriented to the NNE [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -292865     | 252059      | -2564      | 330        |
| 1.5 : 1.0 | -292184     | 251867      | -1883      | 138        |
| 1.4 : 1.0 | -291574     | 251713      | -1273      | -16        |
| 1.3 : 1.0 | -291052     | 251608      | -751       | -121       |
| 1.2 : 1.0 | -290642     | 251563      | -341       | -166       |
| 1.1 : 1.0 | -290376     | 251596      | -75        | -133       |
| 1.0 : 1.0 | -290301     | 251729      | 0          | 0          |
| 1.0 : 1.1 | -290449     | 251963      | -148       | 234        |
| 1.0 : 1.2 | -290781     | 252267      | -480       | 538        |
| 1.0 : 1.3 | -291251     | 252622      | -950       | 893        |
| 1.0 : 1.4 | -291830     | 253016      | -1529      | 1287       |
| 1.0 : 1.5 | -292492     | 253440      | -2191      | 1711       |
| 1.0 : 1.6 | -293220     | 253887      | -2919      | 2158       |

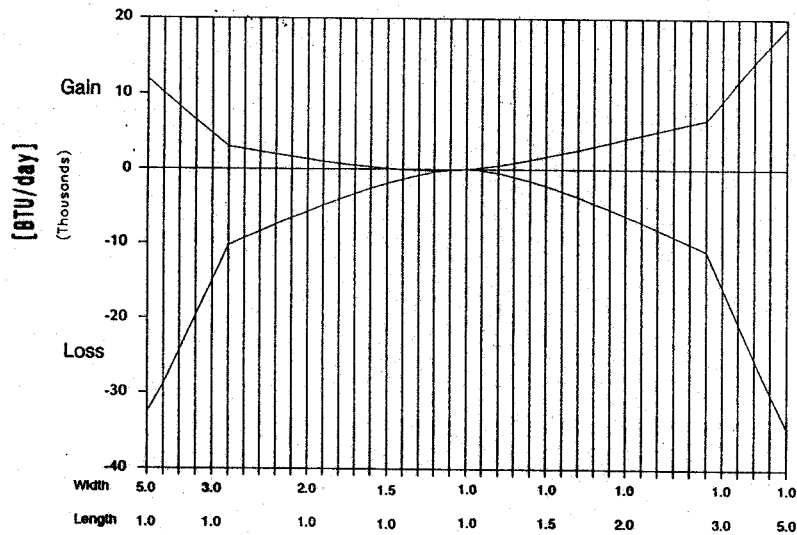


Fig. 6.18 Daily average heat gain and heat loss for the NNE orientation

Table 6.21 Daily average heat gain and heat loss in buildings oriented to the NNW [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -292431     | 253366      | -2770      | 330        |
| 1.5 : 1.0 | -291723     | 253174      | -2062      | 138        |
| 1.4 : 1.0 | -291083     | 253021      | -1422      | -15        |
| 1.3 : 1.0 | -290529     | 252915      | -868       | -121       |
| 1.2 : 1.0 | -290083     | 252871      | -422       | -165       |
| 1.1 : 1.0 | -289779     | 252903      | -118       | -133       |
| 1.0 : 1.0 | -289661     | 253036      | 0          | 0          |
| 1.0 : 1.1 | -289767     | 253271      | -106       | 235        |
| 1.0 : 1.2 | -290059     | 253575      | -398       | 539        |
| 1.0 : 1.3 | -290494     | 253930      | -833       | 894        |
| 1.0 : 1.4 | -291038     | 254324      | -1377      | 1288       |
| 1.0 : 1.5 | -291669     | 254748      | -2008      | 1712       |
| 1.0 : 1.6 | -292368     | 255195      | -2707      | 2159       |

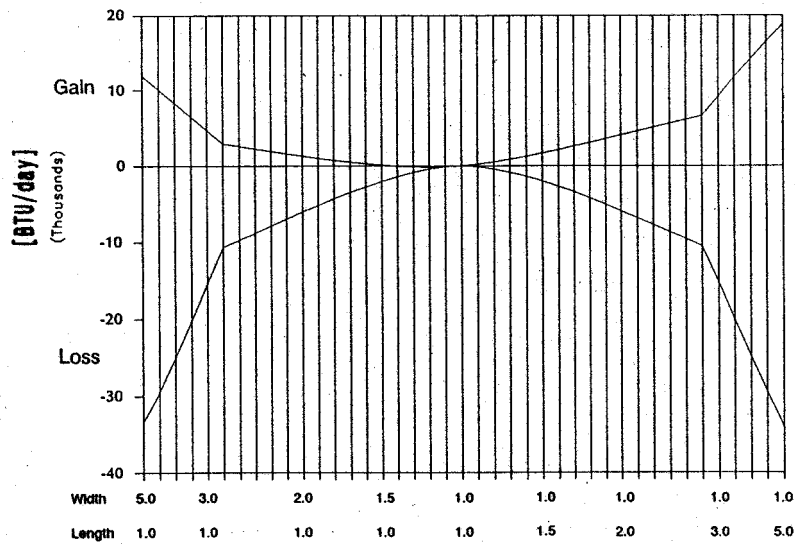
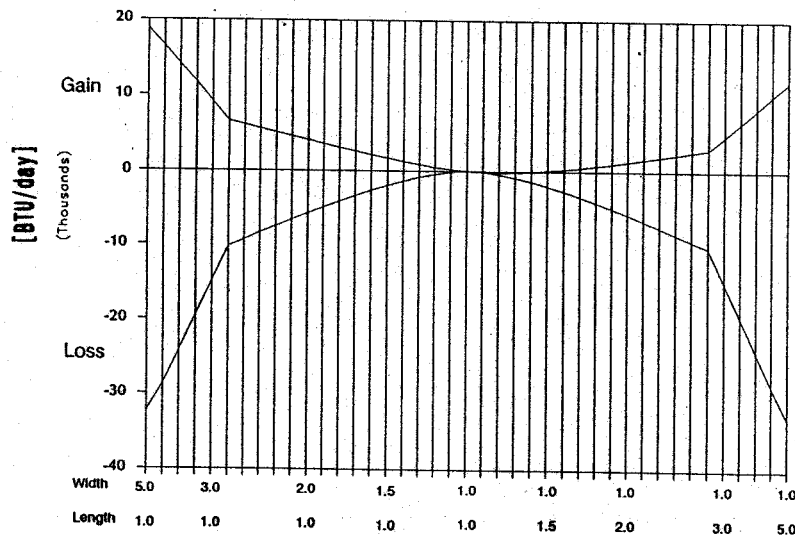


Fig. 6.19 Daily average heat gain and heat loss for the NNW orientation



**Table 6.22 Daily average heat gain and heat loss  
in buildings oriented to the ENE [BTU/day]**

| W : L     | Winter<br>loss | Summer<br>gain | Loss<br>diff. | Gain<br>diff. |
|-----------|----------------|----------------|---------------|---------------|
| 1.6 : 1.0 | -287900        | 264418         | -2630         | 2159          |
| 1.5 : 1.0 | -287221        | 263971         | -1951         | 1712          |
| 1.4 : 1.0 | -286607        | 263547         | -1337         | 1288          |
| 1.3 : 1.0 | -286078        | 263152         | -808          | 893           |
| 1.2 : 1.0 | -285656        | 262797         | -386          | 538           |
| 1.1 : 1.0 | -285372        | 262493         | -102          | 234           |
| 1.0 : 1.0 | -285270        | 262259         | 0             | 0             |
| 1.0 : 1.1 | -285385        | 262126         | -115          | -133          |
| 1.0 : 1.2 | -285680        | 262093         | -410          | -166          |
| 1.0 : 1.3 | -286112        | 262138         | -842          | -121          |
| 1.0 : 1.4 | -286651        | 262243         | -1381         | -16           |
| 1.0 : 1.5 | -287272        | 262396         | -2002         | 137           |
| 1.0 : 1.6 | -287960        | 262588         | -2690         | 329           |



**Fig. 6.20 Daily average heat gain and  
heat loss for the ENE orientation**

Table 6.23 Daily average heat gain and heat loss in buildings oriented to the WNW [BTU/day]

| W : L     | Winter loss | Summer gain | Loss diff. | Gain diff. |
|-----------|-------------|-------------|------------|------------|
| 1.6 : 1.0 | -291691     | 266269      | -2877      | 2158       |
| 1.5 : 1.0 | -290973     | 265822      | -2159      | 1711       |
| 1.4 : 1.0 | -290320     | 265399      | -1506      | 1288       |
| 1.3 : 1.0 | -289749     | 265004      | -935       | 893        |
| 1.2 : 1.0 | -289286     | 264649      | -472       | 538        |
| 1.1 : 1.0 | -288960     | 264346      | -146       | 235        |
| 1.0 : 1.0 | -288814     | 264111      | 0          | 0          |
| 1.0 : 1.1 | -288890     | 263978      | -76        | -133       |
| 1.0 : 1.2 | -289153     | 263946      | 339        | -165       |
| 1.0 : 1.3 | -289558     | 263991      | -744       | -120       |
| 1.0 : 1.4 | -290075     | 264096      | -1261      | -15        |
| 1.0 : 1.5 | -290678     | 264249      | -1864      | 138        |
| 1.0 : 1.6 | -291351     | 264441      | -2537      | 330        |

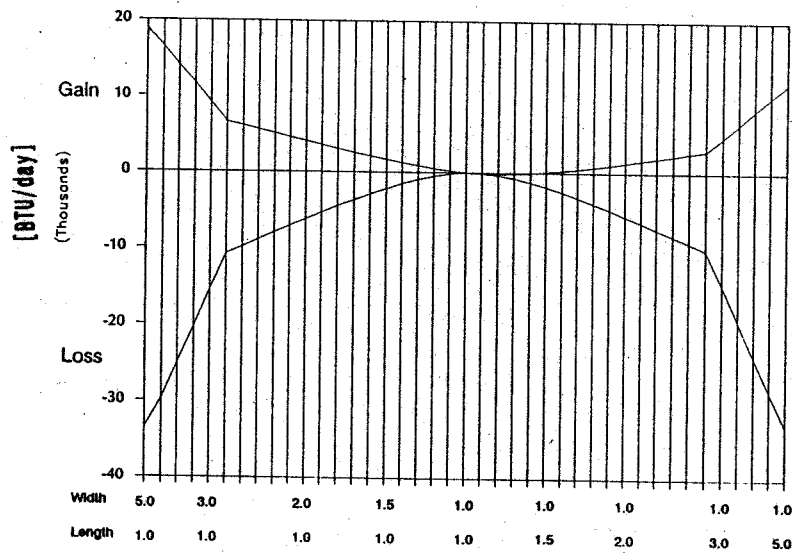


Fig. 6.21 Daily average heat gain and heat loss for the WNW orientation